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# 1 GeV リニアック検討資料

## 1 GeV LINAC DESIGN NOTE

題目 (TITLE) 四極電磁石の概念設計プログラム

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### 概要 (ABSTRACT)

高崎メモによる四極電磁石の概念設計の計算部分をマックで簡単に出来るようにしたので、紹介する(TRUE BASIC 使用)。

### KEY WORDS:

Ion source, RFQ, DTL, CCL, Magnet, Monitor, Beam Dynamics,  
Transport, Vacuum, Cooling  
Klystron, Low level rf, High power rf, Modulator  
Control, Operation, Radiation, Others

# 四極電磁石の概念設計プログラム

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高崎メモによる四極電磁石の概念設計の計算部分をマックで簡単に出来るようにしたので、紹介する。

## 基本式

$$NI = G r^2 / (2 * \mu) \quad [A T]$$
$$\text{flux} = G r^2 (1 + x) / 2 \quad [Tm] : x \text{ is about } 0.5$$
$$\text{pole tip surface mag. field } B_s = G r \leq 1 T$$
$$\text{MORE length} = r / 2 \quad (\text{漏れ磁場の長さ})$$

入力	1	r	bore radius in mm
	2	G	field gradient in T/m
	3	Lq	Q-mag length along z-axis used for computer beam simulation <u>Rmore = r/2 by Takasaki memo</u>
	4	Felength	real pole length along z-axis <u>flux: B in the pole is assumed 1 T ---&gt; mag.half width (width)が 決まる</u>  <u>Bs is smaller than 1T</u> space between two coils > 6 mm by T.K coil space = SPACE

## 冷却条件

$$NI = i * S * f$$

$$s = \text{SPACE} * LL \quad \text{コイル断面積、} f = \text{packing factor}$$

$$\text{空冷 電流密度 } i \quad \frac{1 A/mm^2 \text{ or } 2 A/mm^2}{\text{packing factor} = 0.8}$$

$$\text{水冷 電流密度 } i \quad \frac{10 A/mm^2 \text{ or } 20 A/mm^2}{\text{packing factor} = 0.5}$$

$$\text{コイル断面の形} \quad \text{SPACE} * LL$$

$$LL = NI / (i * f) \quad \text{----> 半径方向の長さをチェックする}$$

## 水冷の場合

入力 5 t,w ホローコンダクターの断面形、w // r 方向

入力 6 thick ホローコンダクターの肉厚

ホロコンの銅断面積 Cuarea

ホロコンの水流部面積 areaWater

ホロコンの電流  $I = i * Cuarea$

ホロコンのターン数  $N = NI / I$  per pole

2層巻を仮定する（宿題：この部分をN巻にして、汎用にして下さい）

絶縁物とコーナーの出っ張りを仮定して全ホロコンの断面積を計算する

全ホロコンの断面積 = wid \* leng

磁石の断面を取り巻く全ホロコンの長さを計算する Lengltum per pole

抵抗をを計算する resis

電力をを計算する power

4 ポールの抵抗 Rtot

4 ポールの電圧 Vtot

4 ポールの電力 Ptot

## 発熱と温度上昇

水温上昇は 10度とする

$$4.2 * V(cc/sec) * \Delta T = P(Watt)$$

流速

## Example of Qmagdesign program

(Below is copy of the output on the screen, Script **bold** is input data)

( This view is not the same as the screen)

ELECTRO Q-MAGNET DESIGN 911112 T. Kato with Takasaki formula and memo

Fundamental equations used for design are

$$NI = G r * r / (2 * \mu) \quad [ A T ]$$

$$\text{flux} = G r * r ( 1 + x ) / 2 : [ T m ] \quad x \text{ is about } 0.5$$

pole tip surface mag. field  $B_s = G r \leq 1 T$

MORE length =  $r / 2$

Please input radius in mm

? **17.5**

----- radius in m = .0175

----- MORE length =  $R / 2 = .00875$

Please input mag.field gradient in T/m

? **45**

----- gradient in T/m = 45

----- pole-tip surface mag. field in T = .7875

-----  $B_s$  is smaller than 1T, ----- OK

-----  $f_{ai}$  in Tm =  $1.03359e-2$

flux : B in the pole is assumed 1 T

----- thus, magnet half-width W in mm = 10.3359

Do you change width? no change =0 else enter in mm

? **17.5**

new width (mm) = 17.5

----- Required NI in AT = 5483.39

Please enter effective Q-magnet length in mm

? **40**

----- effective Q-length in m = .04

----- MORE length in m = .00875

-----  $F_{elength} = L_q - R_{more}$  in m = .03125

Do you agree with  $F_{elength}$ ? If O.K return 0, else enter in mm

? **35**

----- new  $F_{elength}$  in m = .035

half SPACE BETWEEN TWO MAGNET PIECES in mm = 17.5

----- allowed width of coil is (above-3mm) = 14.5

----- COIL AND COOLING DESIGN -----

air cooling current density = 1 A/mm<sup>2</sup>

water cooling current density = 10 - 20 A/mm<sup>2</sup>

$N * I = I * S * f$  f is packing factor = 0.8 is assumed air cooling

$N * I = I * S * f$  f is packing factor = 0.5 is assumed water cooling

s is coil cross area

----- COIL AND COOLING DESIGN-1 WITH AIR -----

--- 1 A/mm2 current density ----

AIR cooling coil cross area is in mm2 = 6854.23

coil width and length in mm= 14.5 472.706

length of coil is too long > 100 mm !!!!!!!

--- 2 A/mm2 current density ----

AIR cooling coil cross area is in mm2 = 3427.12

coil width and length in mm= 14.5 236.353

length of coil is too long > 100 mm !!!!!!!

----- COIL AND COOLING DESIGN-2 WITH WATER -----

water cooling current density = 10 - 20 A/mm2

$N \cdot I = I \cdot S \cdot f$  f is packing factor = 0.5 is assumed water cooling

s is coil cross area

-- 10 A/mm2 WATER cooling coil total cross area is in mm2 = 1096.68

coil width and length in mm= 14.5 75.6329

-- 20 A/mm2 WATER cooling coil total cross area is in mm2 = 548.339

coil width and length in mm= 14.5 37.8165

ENTER HOLOCON YOKO(t),TATE(w) IN mm

? 3.5,6.5

enter thickness in mm

? 1

--- holo conductor design -----

CU-AREA IS IN MM\*\*2= 16.

FOR 10A/mm\*\*2 TOTAL CURRENT/ one holocon IN A = 160.

TURN NUMBER = 34.2712

TURN NUMBER = 34

FOR 20A/mm\*\*2 TOTAL CURRENT/ one holocon IN A = 320.

TURN NUMBER = 17.1356

TURN NUMBER = 18

TWO LAYER WINDING IS ASSUMED, then 2\*t is azimuthal width

10A/mm\*\*2 two layer wid\*Len in mm = 12.5 120.5

20A/mm\*\*2 two layer wid\*Len in mm = 12.5 64.5

Fe pole cross section Felength and half width = 35 17.5

Holocon total length/pole in m= 7.43036 3.93372

total resistance	current	voltage	power
.031579	160.	5.05264	808.423
1.67183e-2	320.	5.34986	1711.95

Increase in water temperature is assumed 10 degrees

$4.2 \cdot V(\text{cc/sec}) \cdot \Delta T = P(\text{Watt})$  is used

Then, required amount of water cc/min = 1154.89 2445.65

Water velocity in m/sec = 2.85158 6.03864

Do you want sum of the result? If yes, enter 1

? 1

\*\*\*\*\* ----- Summary of the electro-quadrupole magnet design ----- \*\*\*\*\*

boreradius (mm) = 17.5  
 gradient (T/m) = 45 Bs (T) = .7875 Half flux (T) = 1.03359e-2  
 B in the pole is assumed 1 T  
 magnet half-width W (mm) = 17.5  
 Required NI (AT) = 5483.39  
 effective Q-length (mm) = 40  
 MORE length (mm) = 8.75 Felength=Lq-Rmore (mm) = 35  
 allowed width of coil(mm)= 14.5

----- COIL AND COOLING DESIGN-1 WITH AIR -----

	1 A/mm2	2 A/mm2
current density	1 A/mm2	2 A/mm2
Total coil cross area (mm2)	6854.23	1713.56
coil width (mm)	14.50	14.50
coil length (mm)	472.71	236.35

----- COIL AND COOLING DESIGN-2 WITH WATER -----

	10 A/mm2	20 A/mm2
current density	10 A/mm2	20 A/mm2
Total cooling coil area (mm2)	1096.68	548.34
coil width (mm)	14.50	14.50
coil length (mm)	75.63	37.82

width and length mean cross section of one side of Fe

-----HOLOCON and Power design-----

Holocon geometry (t w) and thickness (mm)	3.50	6.50	1.00
Cu area and water area of a holocon (mm2)	16.000	6.75	
turn/pole width length length/turn Tot.coil length/pole			
	mm	mm	m
10A/mm2	34	12.50	120.50
20A/mm2	18	12.50	64.50
			.22
			.22
			7.43
			3.93
7.43036			

	total resist	current	voltage	power	water volume	velocity
	ohm	A	V	W	cc/min	m/sec
10A/mm2	.0315790	160	5.05	808.42	1154.89	2.85
20A/mm2	.0167183	320	5.35	1711.95	2445.65	6.04